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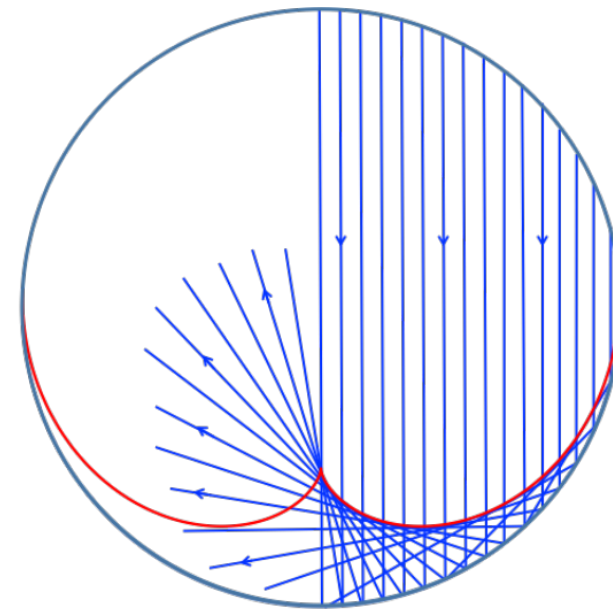
# Singularities of particle trajectory caustics and beam shaping in bunch compressors

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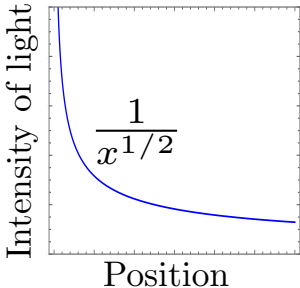
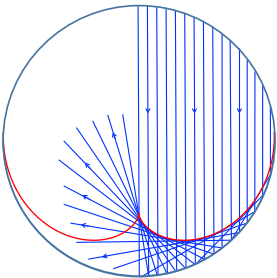
# Caustics



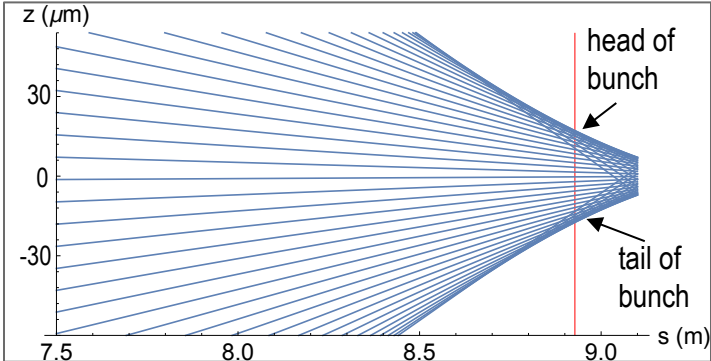
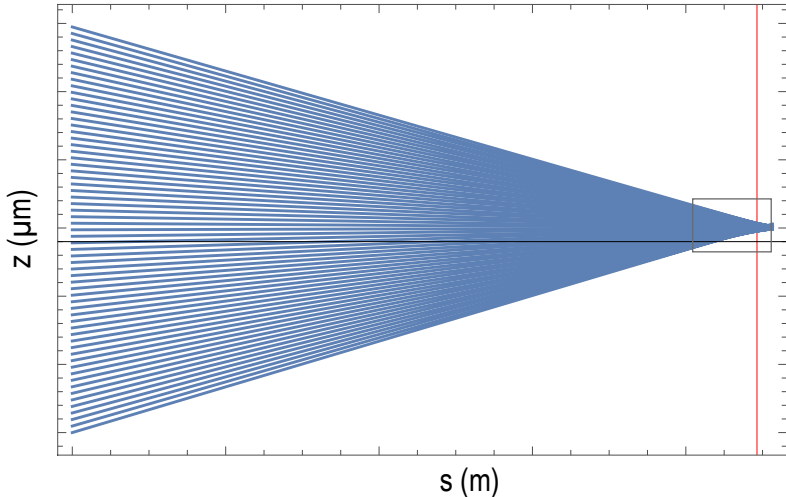
# Caustics



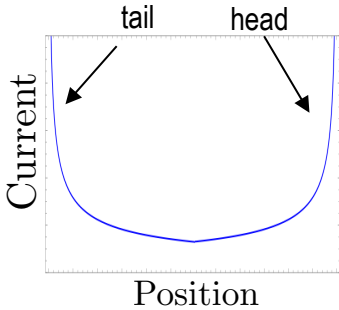
Optical caustics:



Electron trajectories caustics:



*These current horns are a manifestation of the caustic nature of the electron trajectories, as singularities of families of trajectories are encountered.*



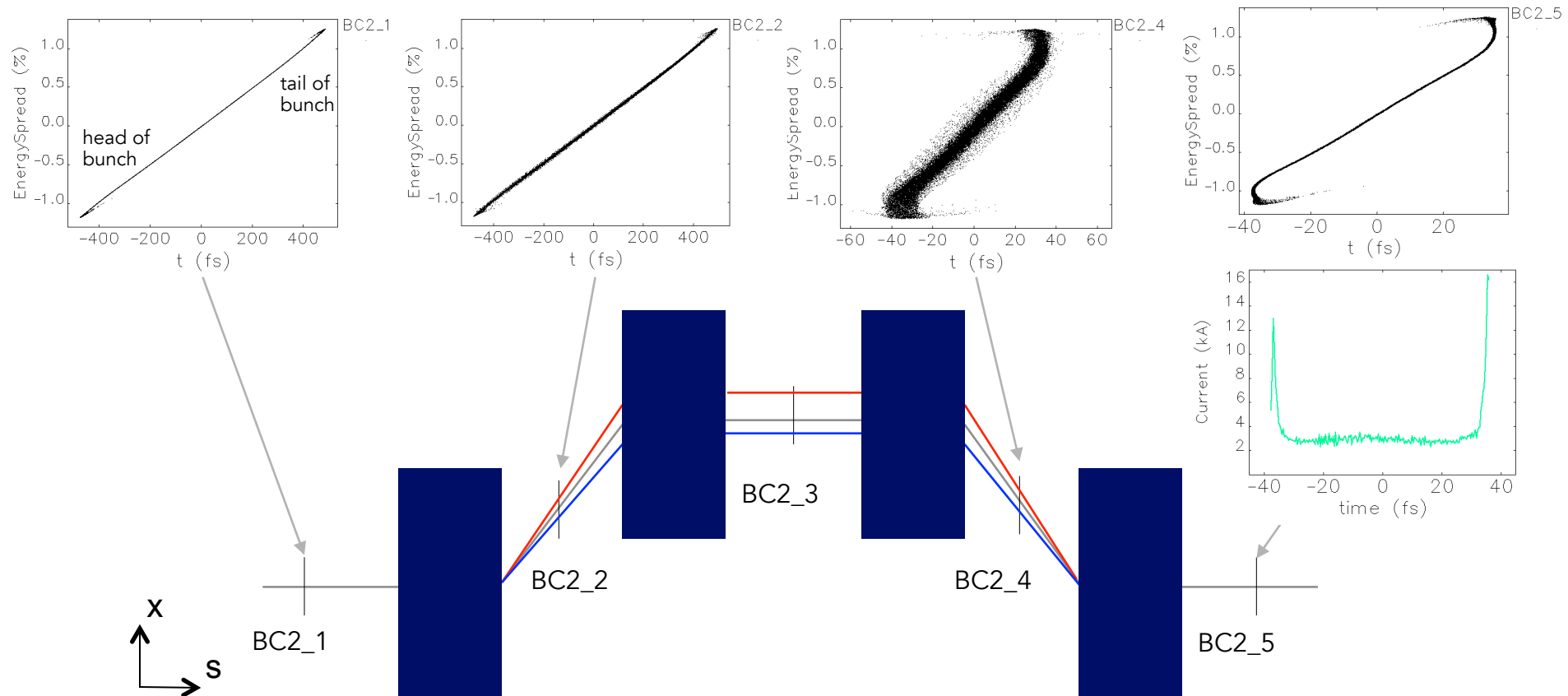
# Caustics / Catastrophe theory



Image: EC Zeeman (1976) Catastrophe Theory in Scientific American.

# Current horns

- Current horns are resultant from caustics



# Caustic expression

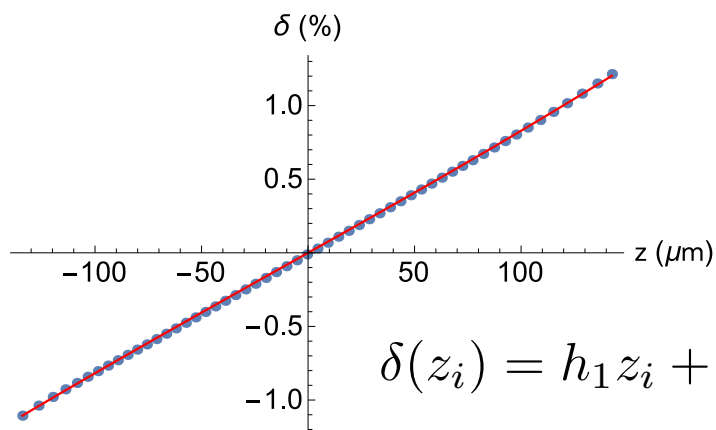


- Expression for caustics:

$$\tilde{z}(z_i) = z_i + \frac{\delta(z_i)(-1 + T_{566}(-2 + \delta(z_i))\delta'(z_i) + U_{5666}(-3 + \delta(z_i)^2)\delta'(z_i))}{\delta'(z_i)}$$

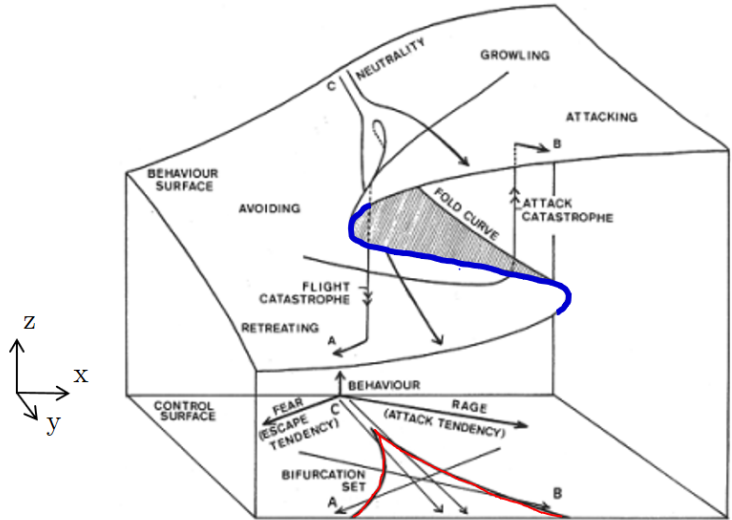
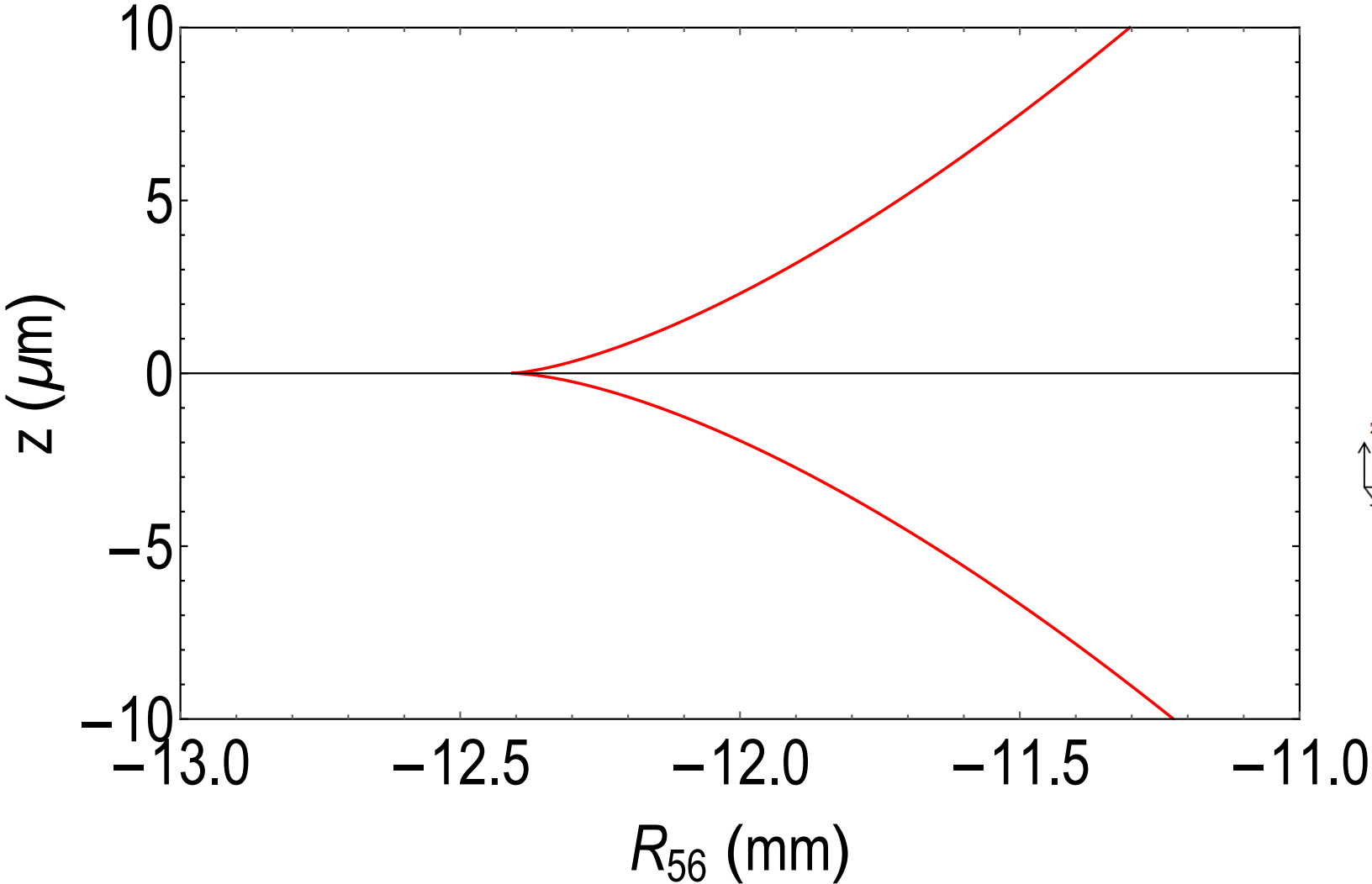
$$\tilde{R}_{56}(z_i) = \frac{-1 - 2T_{566}\delta'(z_i) - 3U_{5666}\delta'(z_i)}{\delta'(z_i)}$$

Initial longitudinal phase space distribution:

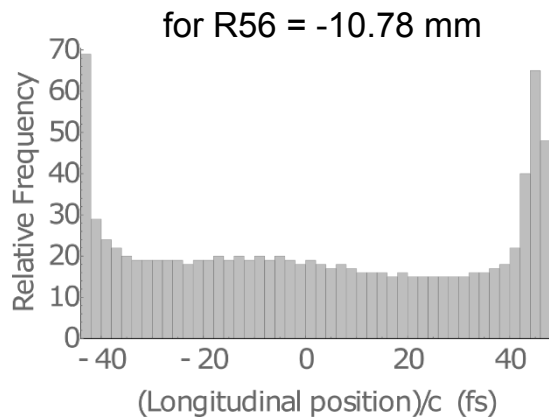
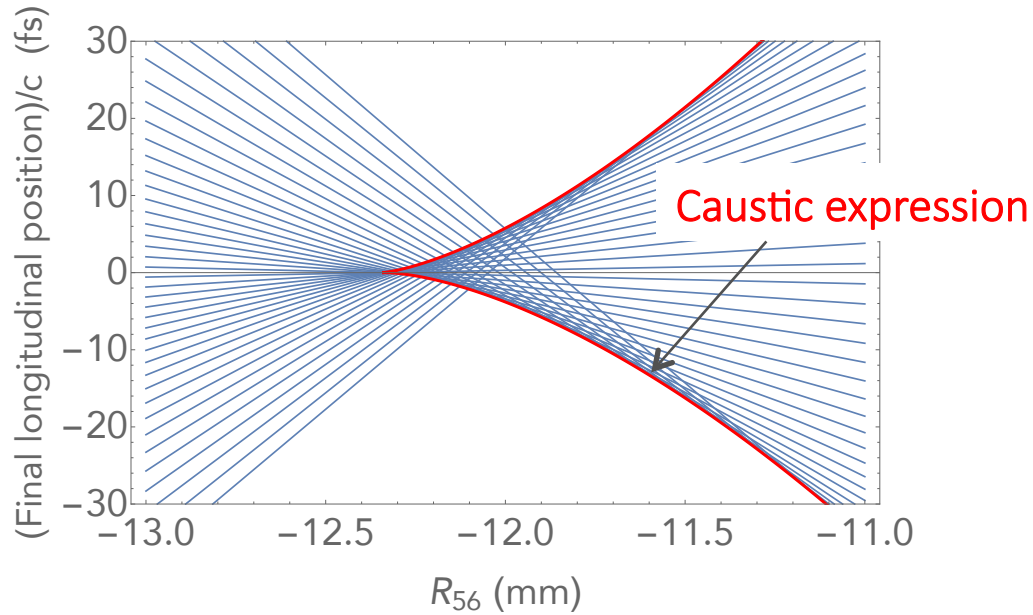


T. K. Charles et al. (2016) Phys. Rev. AB, **19**, 104402

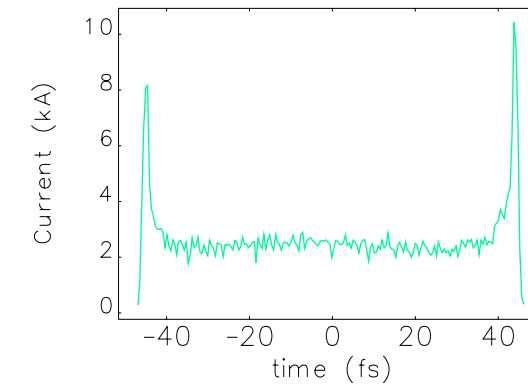
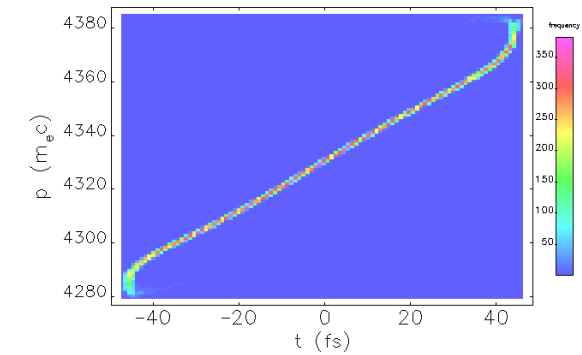
# Caustic expression



# Comparison with simulations



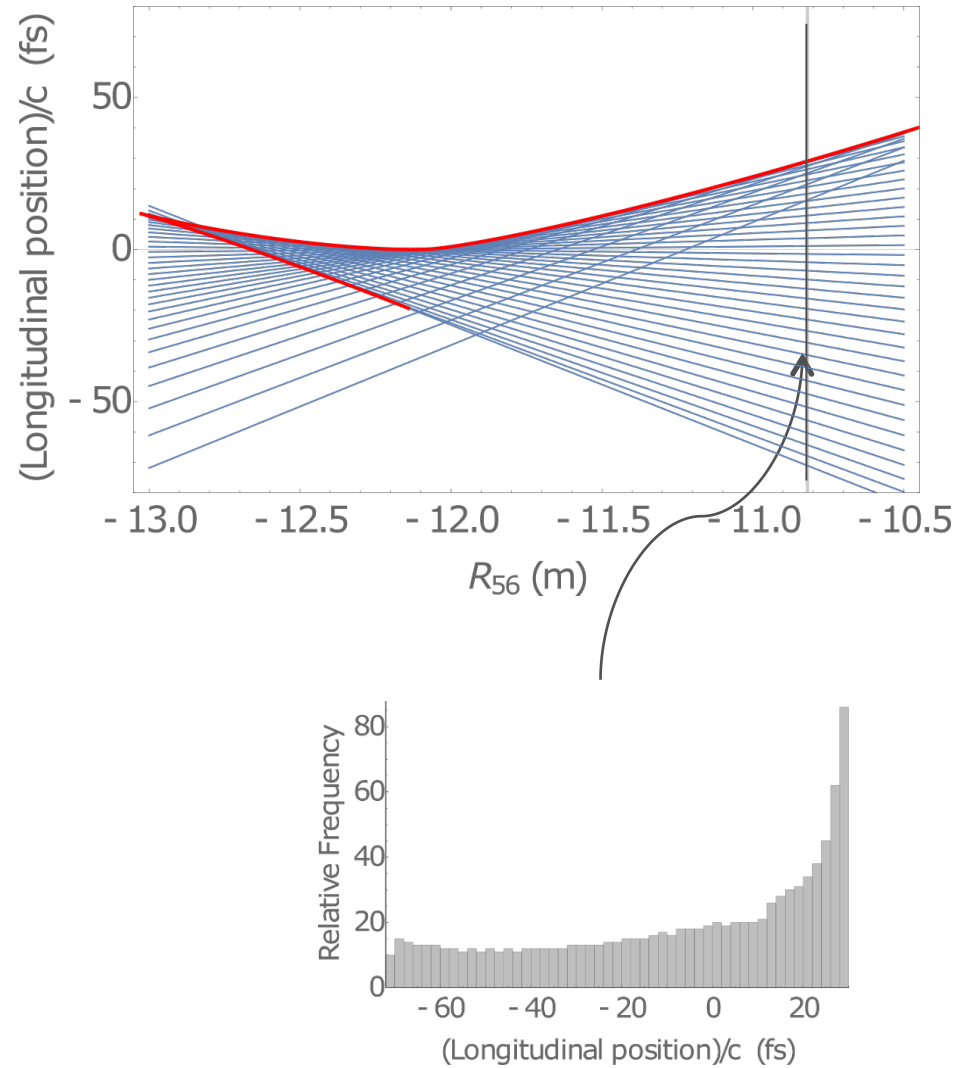
ELEGANT simulation results:



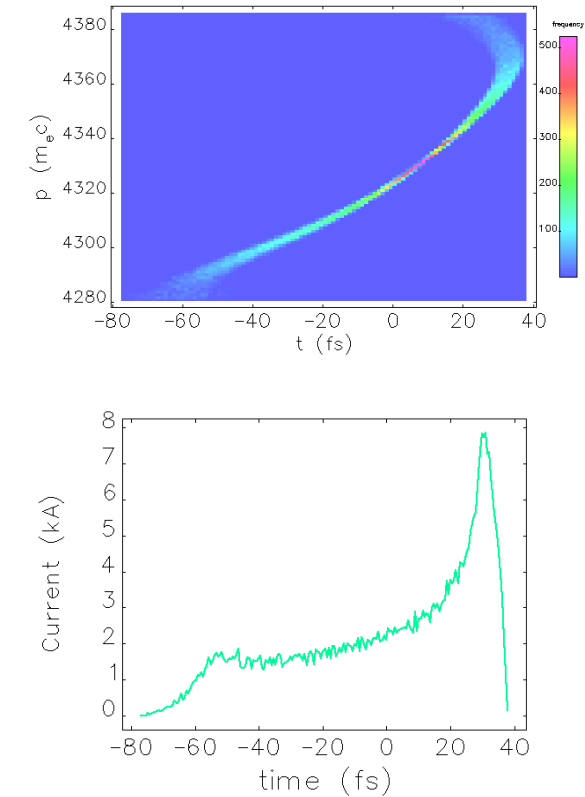
Double-horned current structure produced at the end of a dispersive region where  $R_{56} = -10.78$  mm,  $T_{566} = 16.35$  mm and  $U_{5666} = -11.38$  mm.



# Comparison with simulations

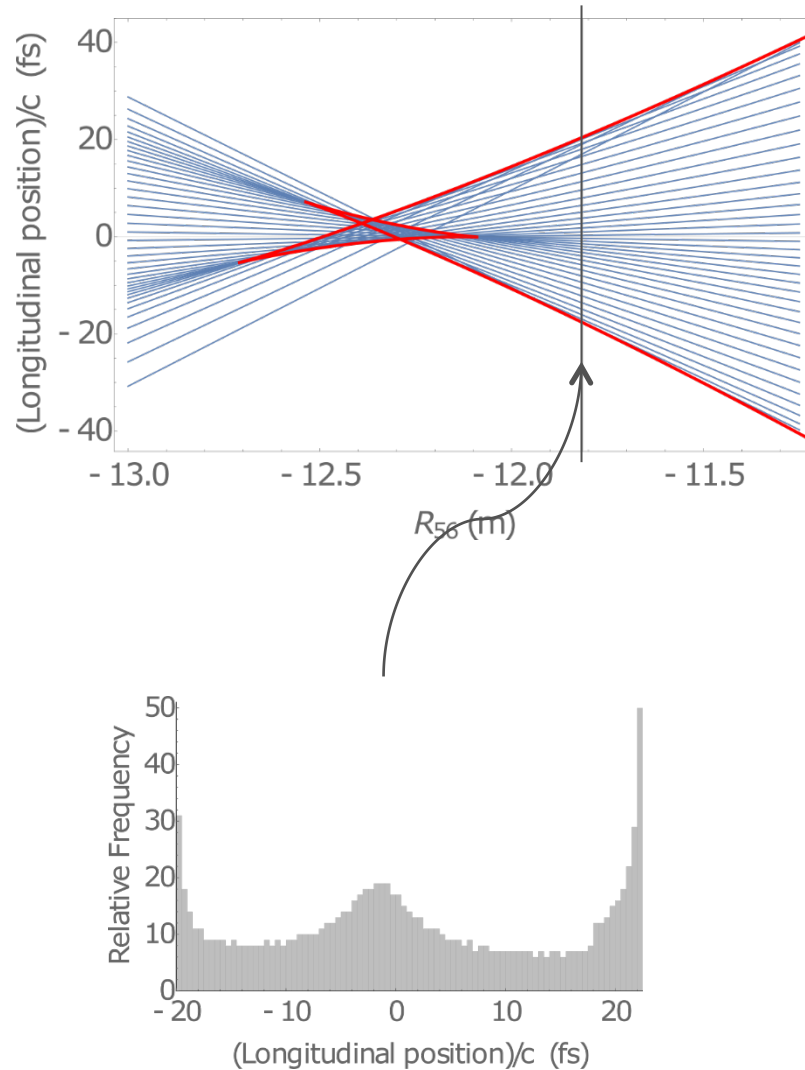


ELEGANT simulation results:

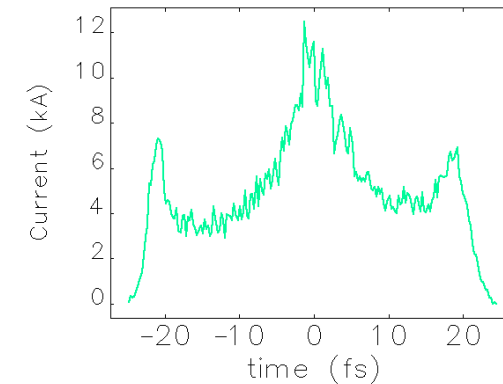
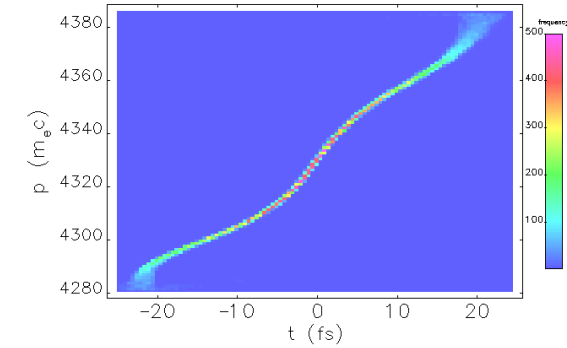


Single-horn current profile produced with  $R_{56} = -10.82$  mm,  $T_{566} = -41.07$  mm and  $U_{5666} = 0.40$  m

# Comparison with simulations



ELEGANT simulation results:



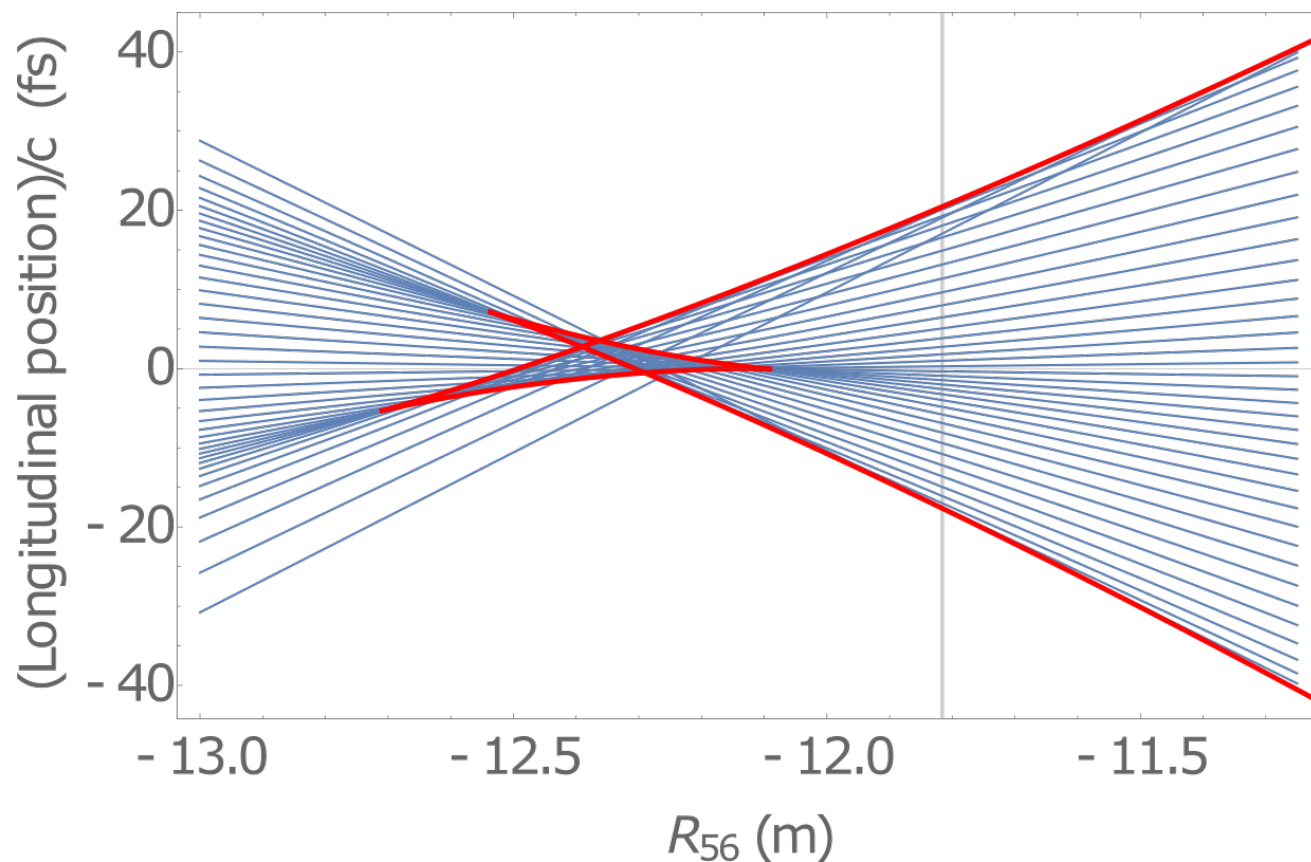
Current profile produced with  $R_{56} = -11.76$  mm,  $T_{566} = 16.10$  mm and  $U_{5666} = 2.60$  m.

# A closer look...

$$\tilde{z}(z_i) = z_i + \frac{\delta(z_i)(-1 + T_{566}(-2 + \delta(z_i))\delta'(z_i) + U_{5666}(-3 + \delta(z_i)^2)\delta'(z_i))}{\delta'(z_i)}$$

$$\tilde{R}_{56}(z_i) = \frac{-1 - 2T_{566}\delta'(z_i) - 3U_{5666}\delta'(z_i)}{\delta'(z_i)}$$

Three types of catastrophes  
but all described by the same  
parametric expression.





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# Can we avoid caustic current horns?

# Caustic condition



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Caustics condition:

$$R_{566} s \left. \frac{d(\delta(z))}{dz} \right|_{z=z_i} + T_{566} s \left. \frac{d}{dz} (\delta^2(z)) \right|_{z=z_i} + U_{5666} s \left. \frac{d}{dz} (\delta^3(z)) \right|_{z=z_i} + s_{BC} = 0.$$

where,

$\delta$  = energy spread

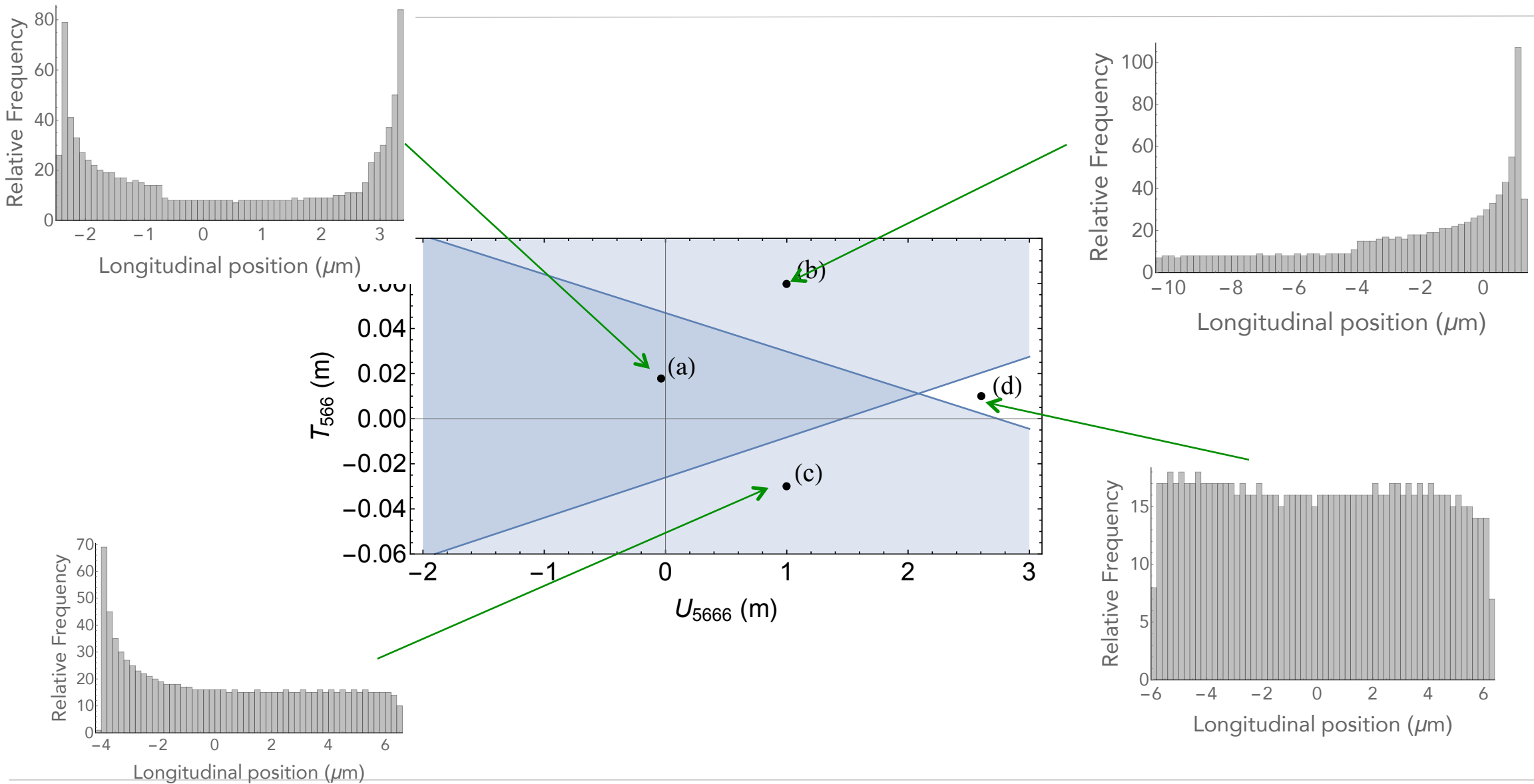
$z_i$  = initial longitudinal position

$s$  = position along accelerator

$s_{BC}$  = end of bunch compressor position

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# Avoiding caustics

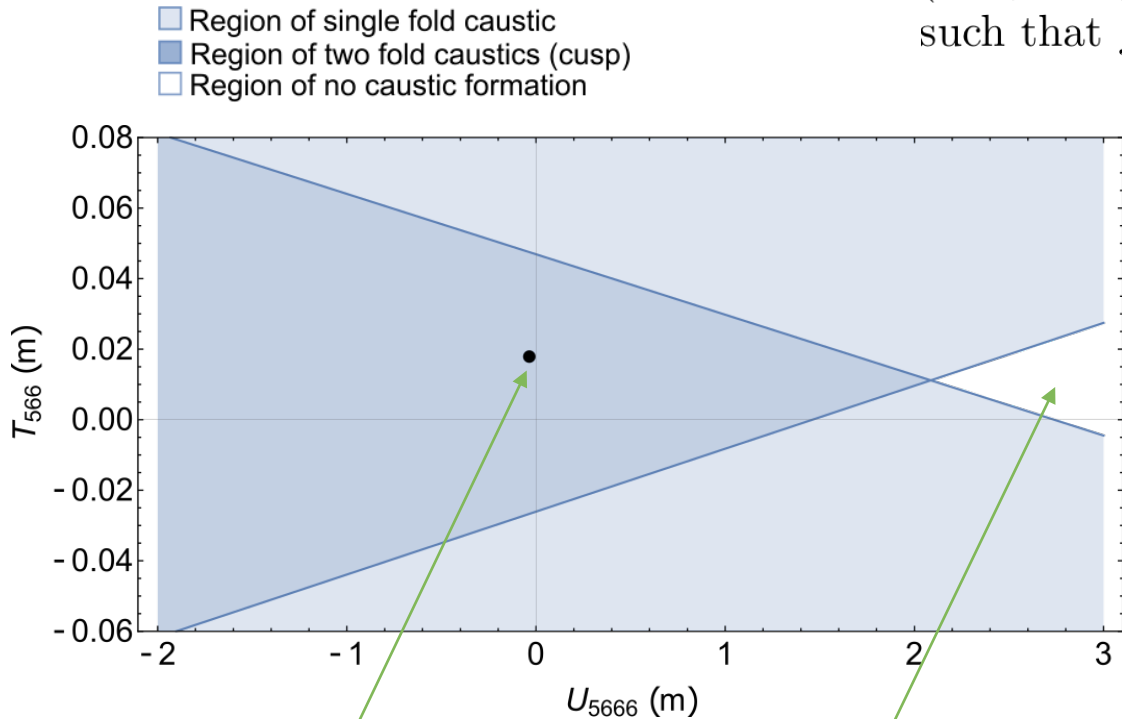


# Boundaries between caustic regions



The border between the caustic regions is defined by the set of variables,  $(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3)$ , evaluated for a given initial bunch with  $z_{\min/\max}$ , such that  $f(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3; z_{\min/\max}) = 0$ , with,

$$f(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3; z_{\min/\max}) = 1 + h_1 R_{56} + 2h_2 R_{56} z_{\min/\max} + 3h_3 R_{56} z_{\min/\max}^2 + 2T_{566} h_1^2 z_{\min/\max} + 6T_{566} h_1 h_2 z_{\min/\max}^2 + 3h_1^3 U_{5666} z_{\min/\max}^2.$$

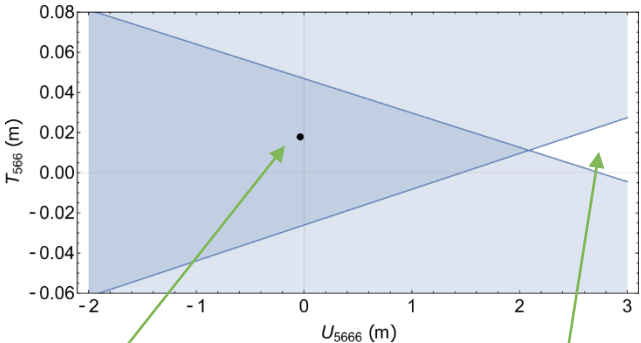


Typical working point of a 4-dipole chicane

Where we'd prefer to be (non-caustic region).

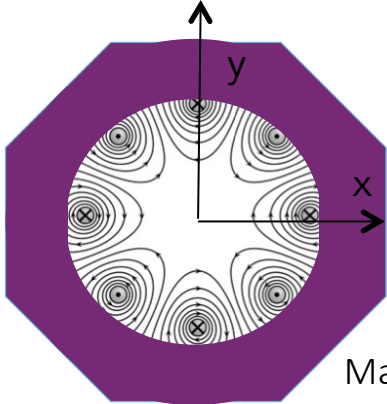
Considering a BC where the entrance bunch is characterized by  $h_1, h_2$ , and  $h_3$  (i.e. the first, second and third order chirp), for a given value of  $R_{56}$ , the values of  $T_{566}$  and  $U_{5666}$  can be chosen to ensure the working point is within the non-caustic region.

# Using octupoles to alter U5666

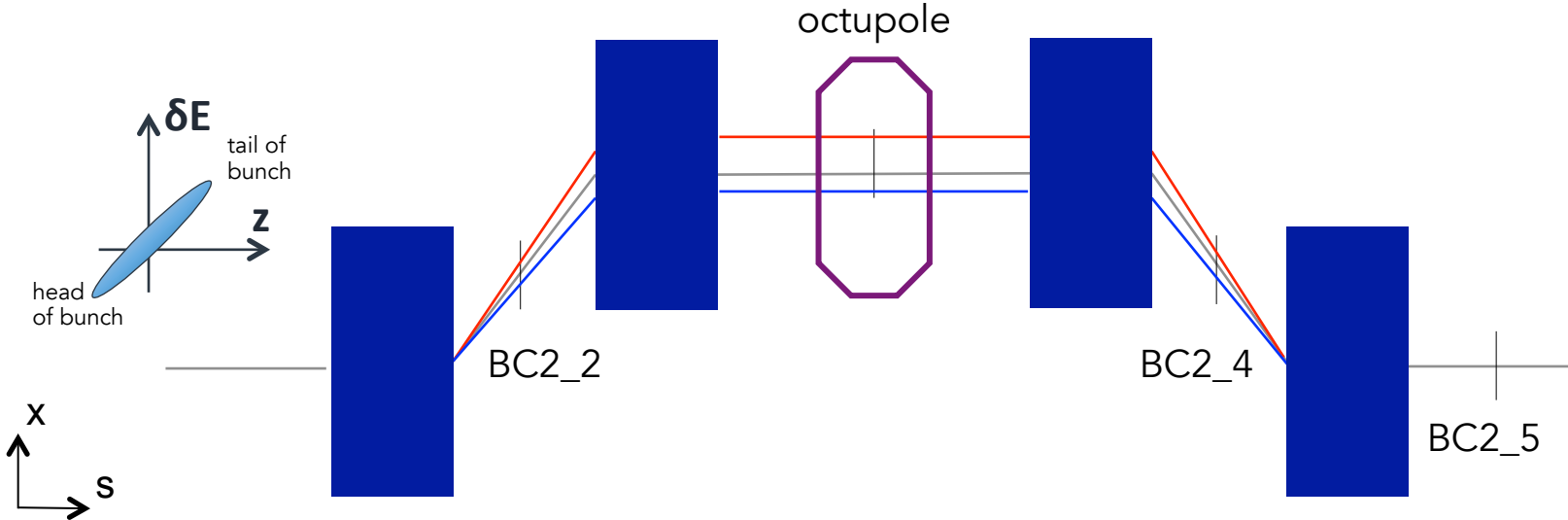


Typical working point of a 4-dipole chicane

Where we'd prefer to be (non-caustic region).



Magnetic field varies as  $x^3$  and  $y^3$





# Boundaries between caustic regions



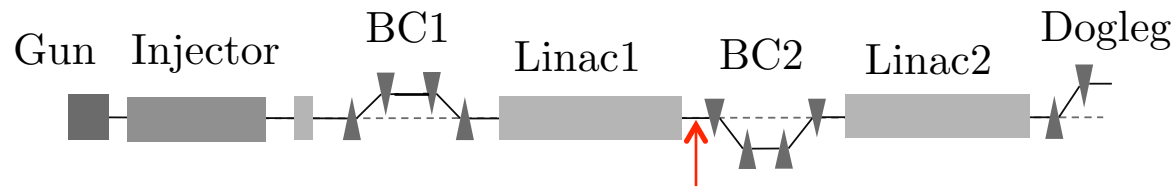
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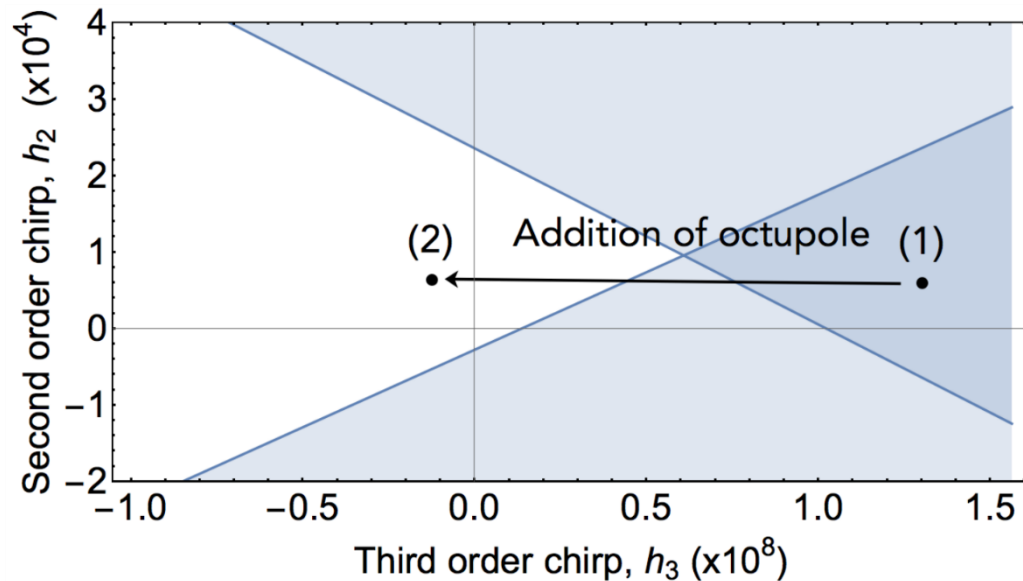
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The border between the caustic regions is defined by the set of variables,  $(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3)$ , evaluated for a given initial bunch with  $z_{\min/\max}$ , such that  $f(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3; z_{\min/\max}) = 0$ , with,



$$f(R_{56}, T_{566}, U_{5666}, h_1, h_2, h_3; z_{\min/\max}) = 1 + h_1 R_{56} + 2h_2 R_{56} z_{\min/\max} + 3h_3 R_{56} z_{\min/\max}^2 + 2T_{566} h_1^2 z_{\min/\max} + 6T_{566} h_1 h_2 z_{\min/\max}^2 + 3h_1^3 U_{5666} z_{\min/\max}^2.$$

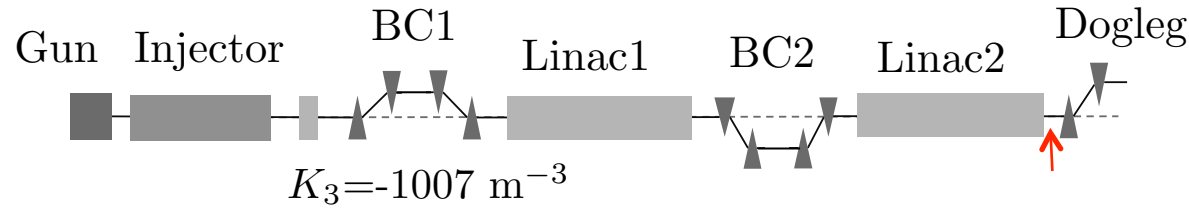


Two cases were investigated:

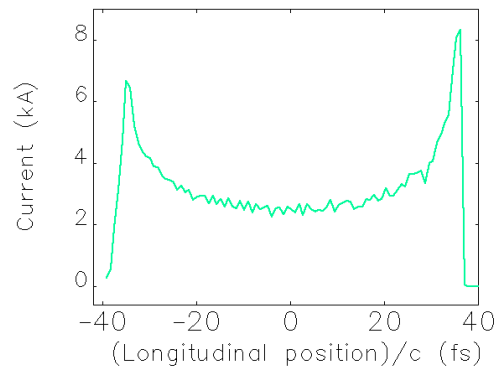
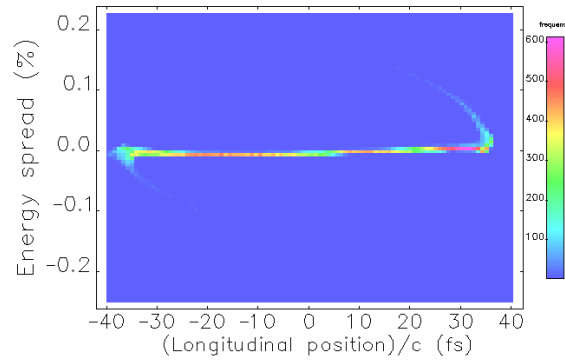
1. Predominately **S-band** linac
2. Predominately **X-band** linac

# FEL, S-band linac simulations

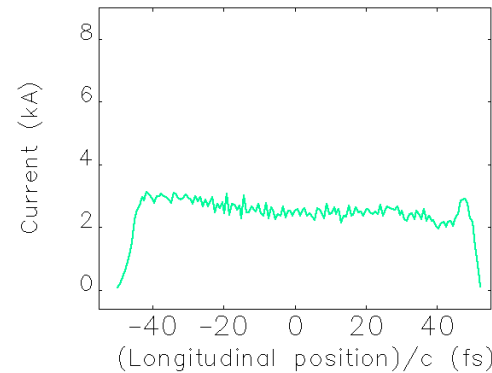
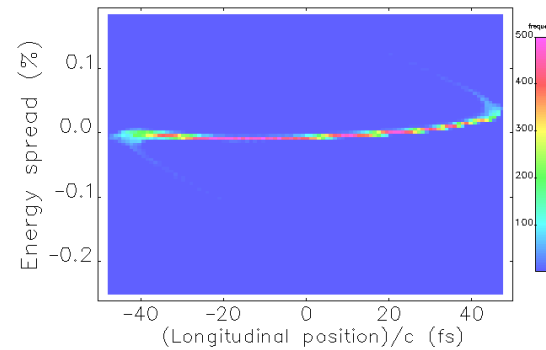
S-band Linac



*Without* octupole:



*With* octupole:



The caustic current-horns have been prevented from forming.

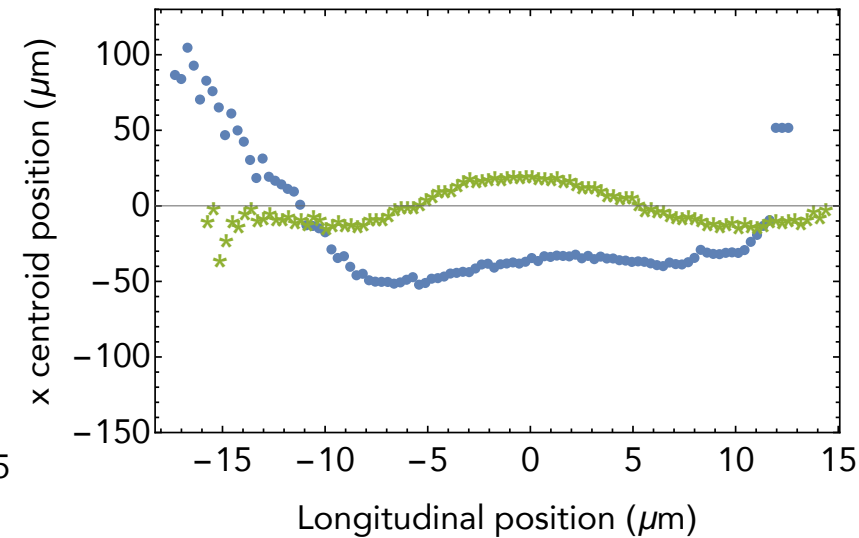
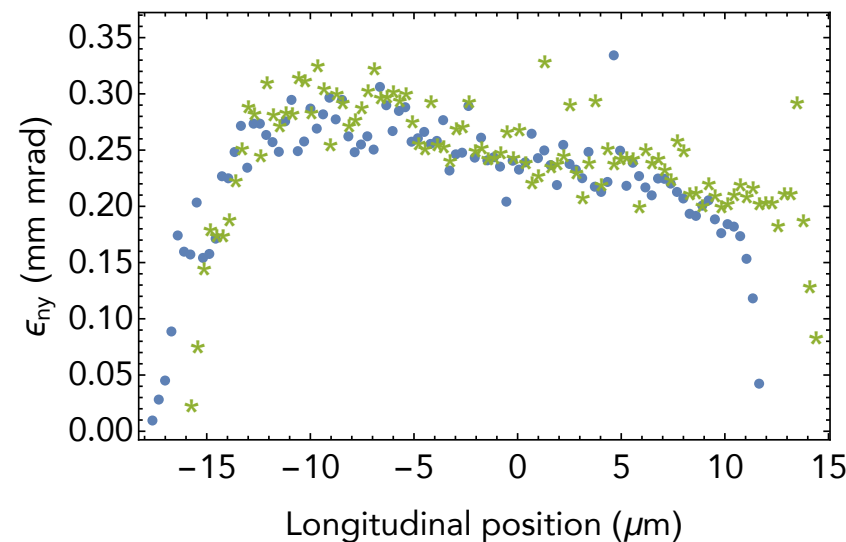
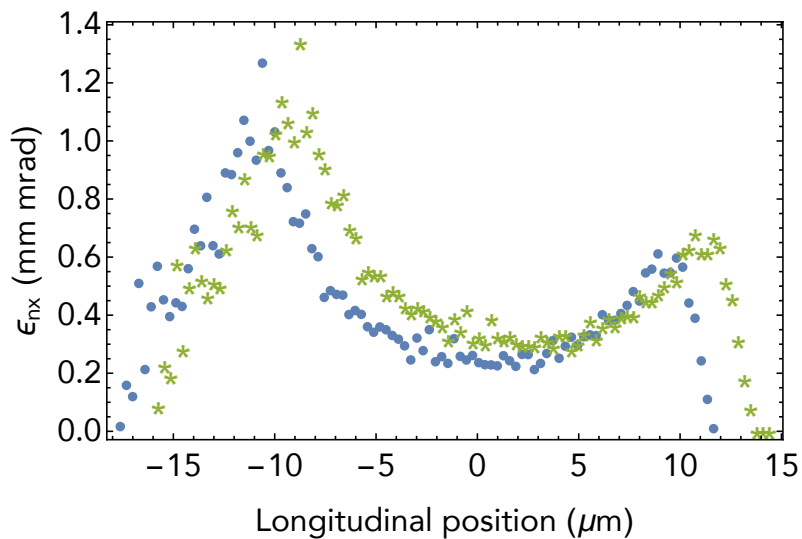
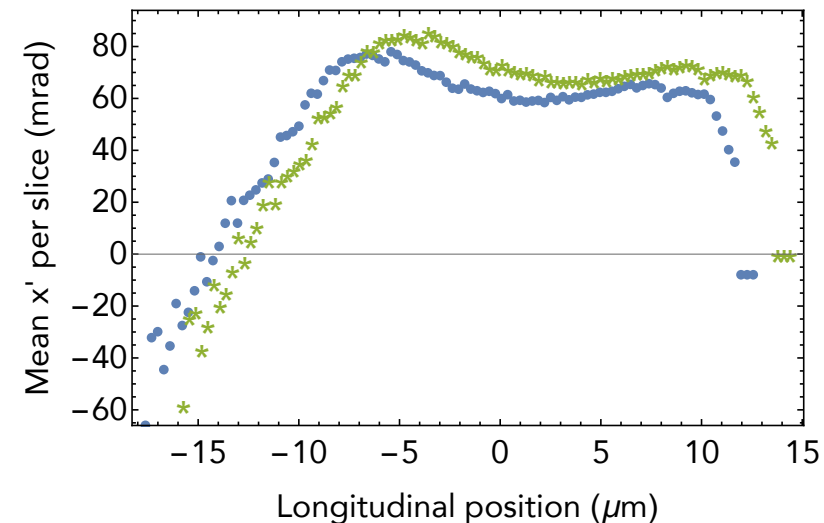
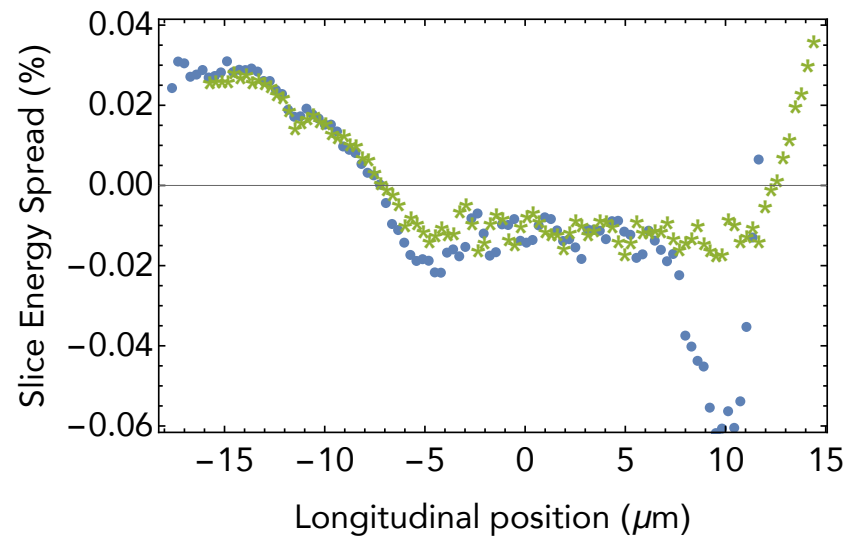
# Slice properties



## S-band linac

*Without* octupole: ●

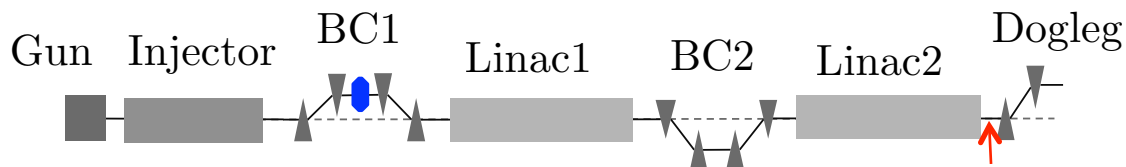
*With* octupole: \*



# Avoiding caustics, X-band linac



X-band Linac



$$R_{56} = -82.38 \text{ mm}$$

$$T_{566} = 102.40 \text{ mm}$$

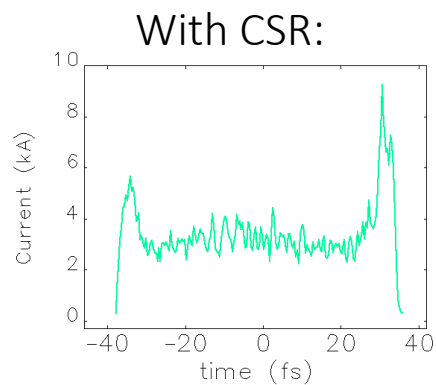
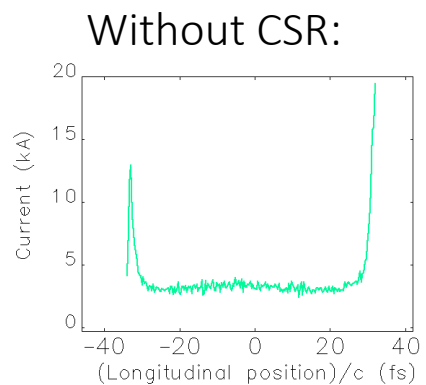
$$U_{5666} = -5.23 \text{ m}$$

$$R_{56} = -11.18 \text{ mm}$$

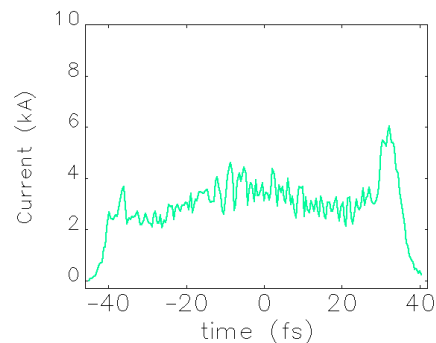
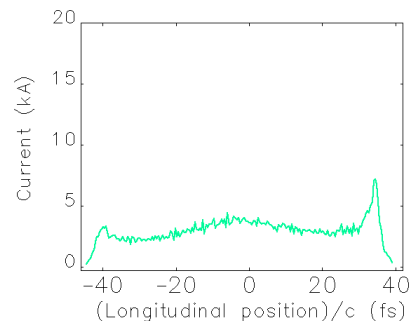
$$T_{566} = 16.77 \text{ mm}$$

$$U_{5666} = -11.10 \text{ mm}$$

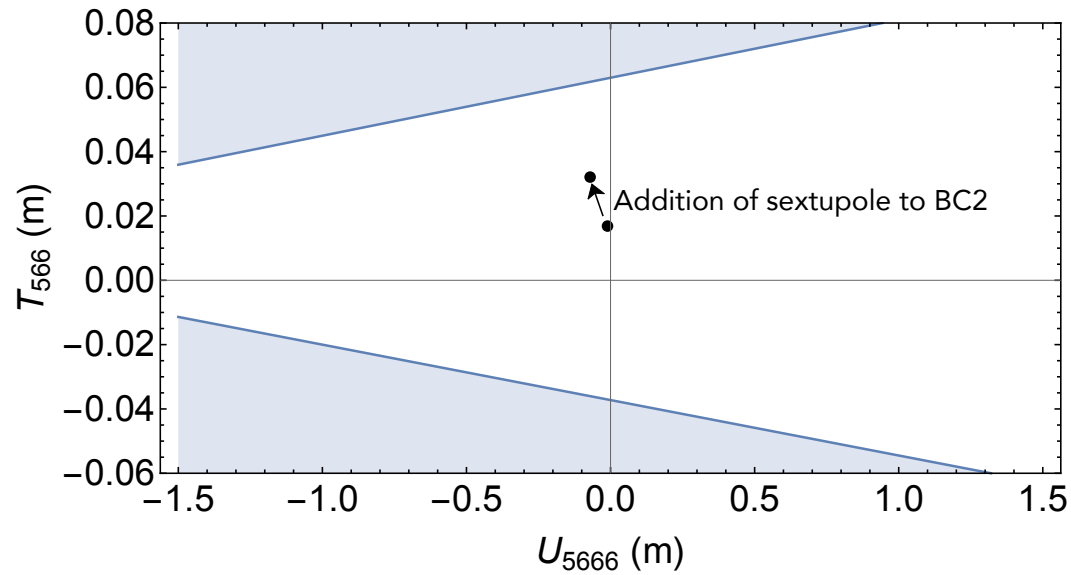
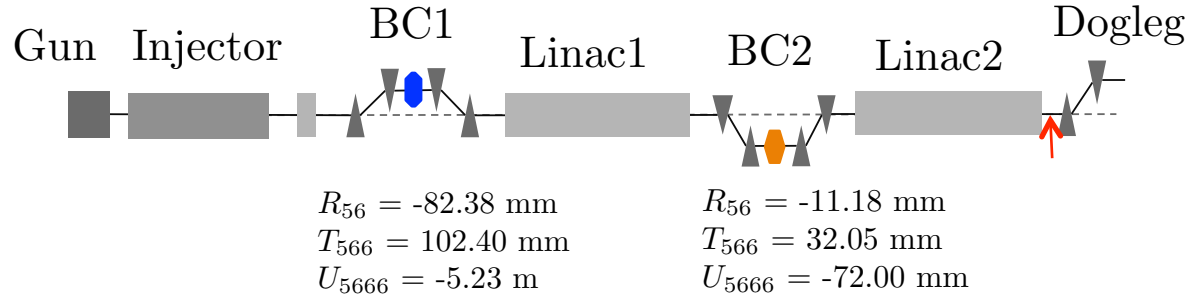
Without octupole:



With octupole:



# Further optimisation

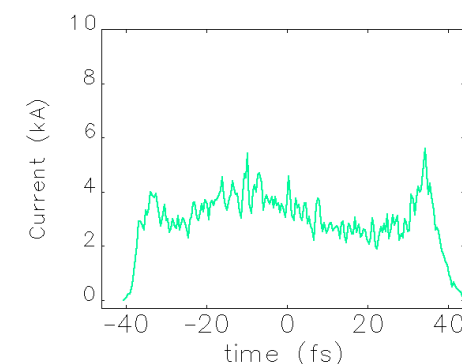
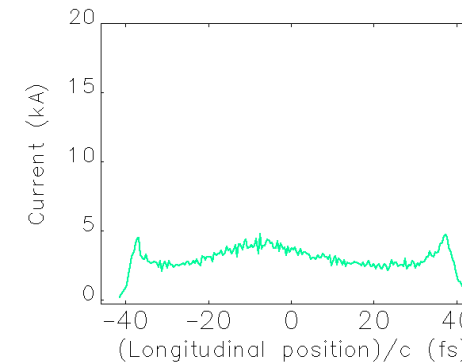
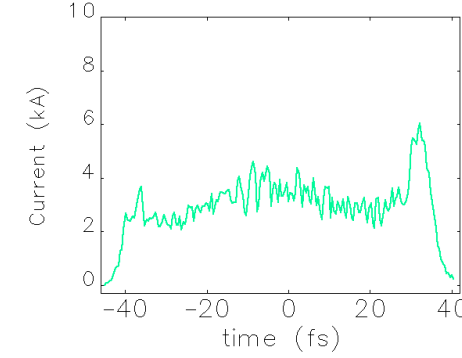
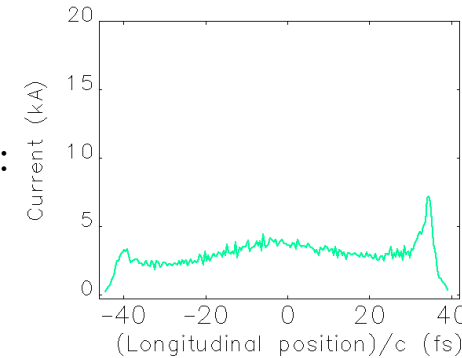


Without sextupole:

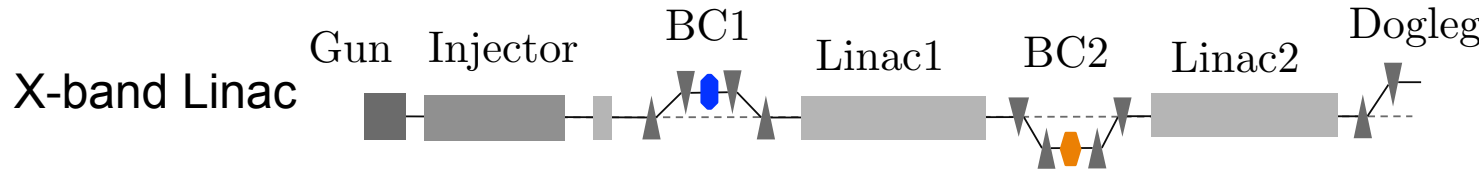
With sextupole:

Without CSR:

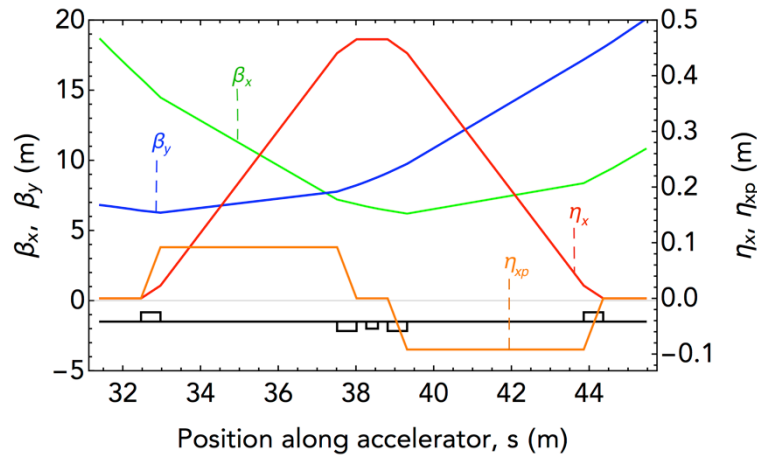
With CSR:



# FEL, X-band linac



Bunch Compressor 1



BC1:

$$R56 = -82.36 \text{ mm}$$

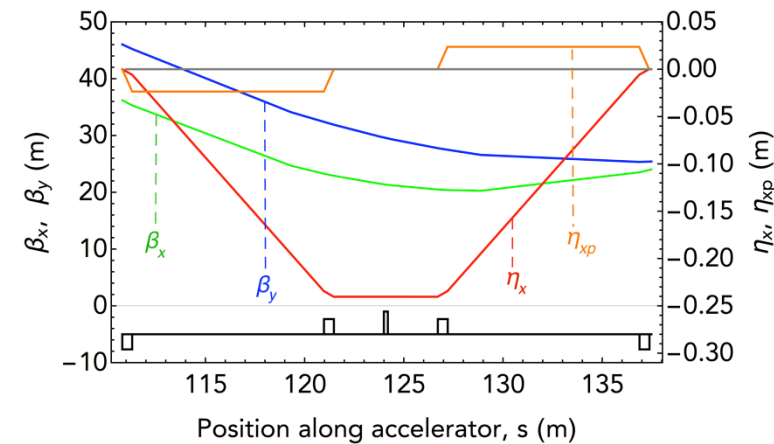
$$T566 = 102.40 \text{ mm}$$

$$U5666 = -5.23 \text{ m}$$

Dipole bending angle,  $\theta = 5.25^\circ$

Octupole strength,  $K3 = 2061 \text{ m}^{-3}$

Bunch Compressor 2



BC2:

$$R56 = -11.18 \text{ mm}$$

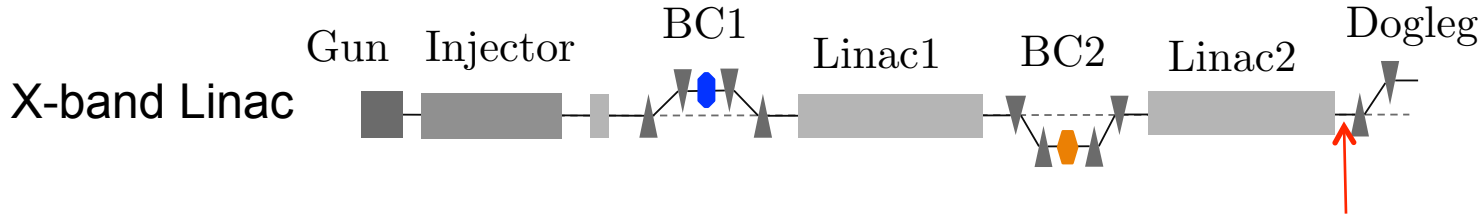
$$T566 = 32.10 \text{ mm}$$

$$U5666 = -72.19 \text{ mm}$$

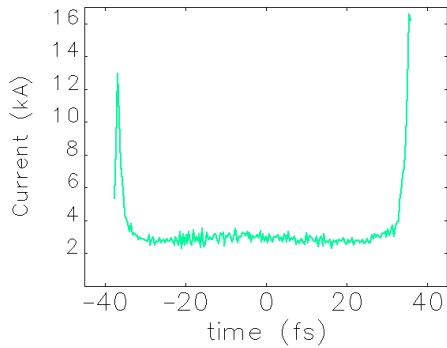
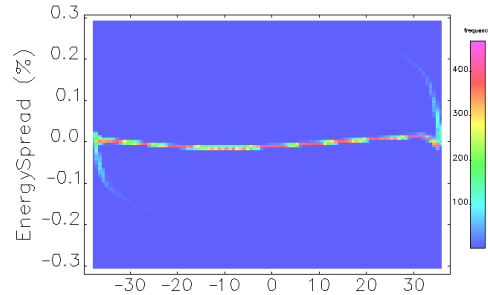
Dipole bending angle,  $\theta = 1.35^\circ$

Sextupole 1 strength,  $K2 = 11.03 \text{ m}^{-2}$

# FEL, X-band linac

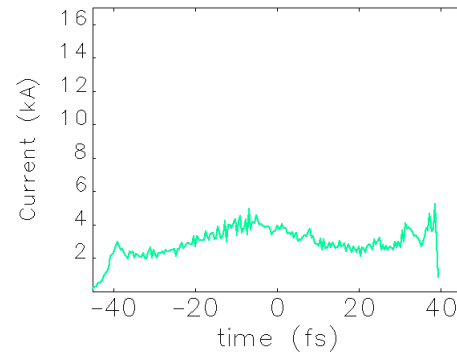
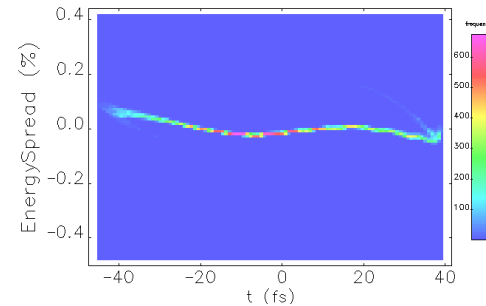


Without octupole & sextupole:



$$\epsilon_{nx} = 1.394 \text{ mm mrad}$$

With octupole & sextupole:



$$\epsilon_{nx} = 0.842 \text{ mm mrad}$$

49% reduction in the CSR-induced emittance growth.

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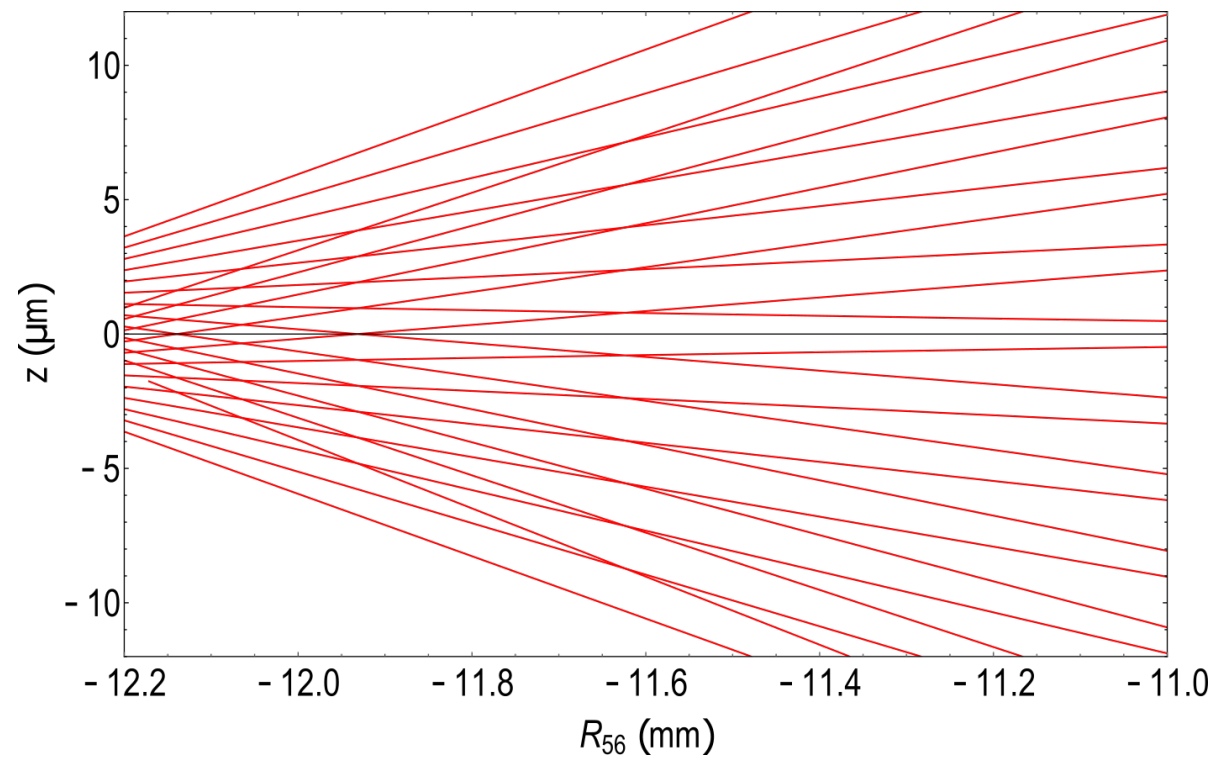
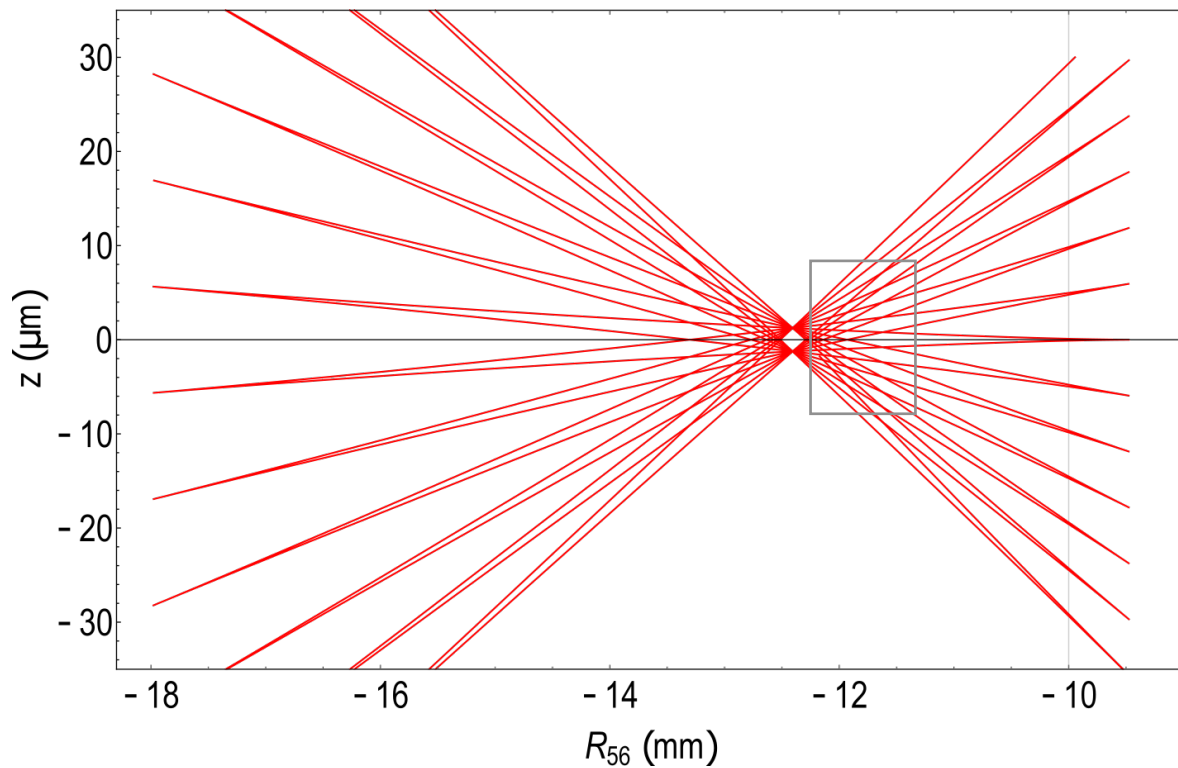
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# Microbunching

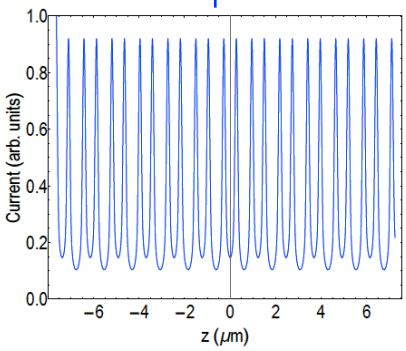
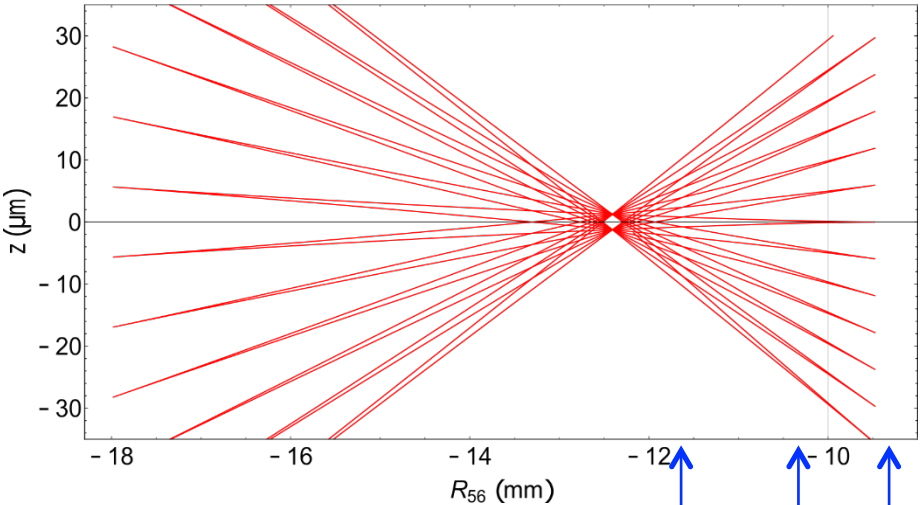
– also a caustic phenomenon?

# Microbunching is also a caustic phenomenon

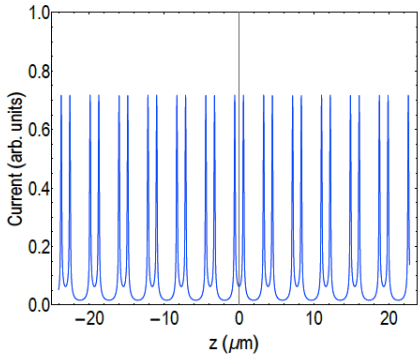
- A caustic expression can also be derived for microbunching. Each line shows where a current spike will be seen.



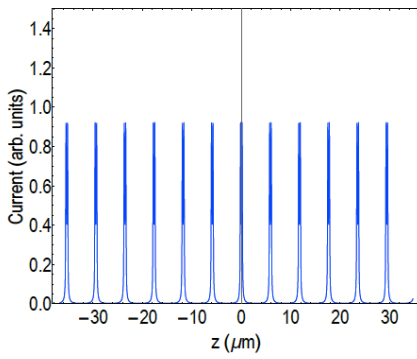
# Microbunching is also a caustic phenomenon



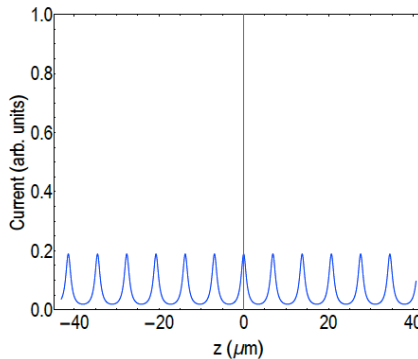
(d)  $R_{56} = -11.8$  mm



(c)  $R_{56} = -10.5$  mm



(b)  $R_{56} = -9.5$  mm



(a)  $R_{56} = -9.0$  mm

# Microbunching – with higher-order effects



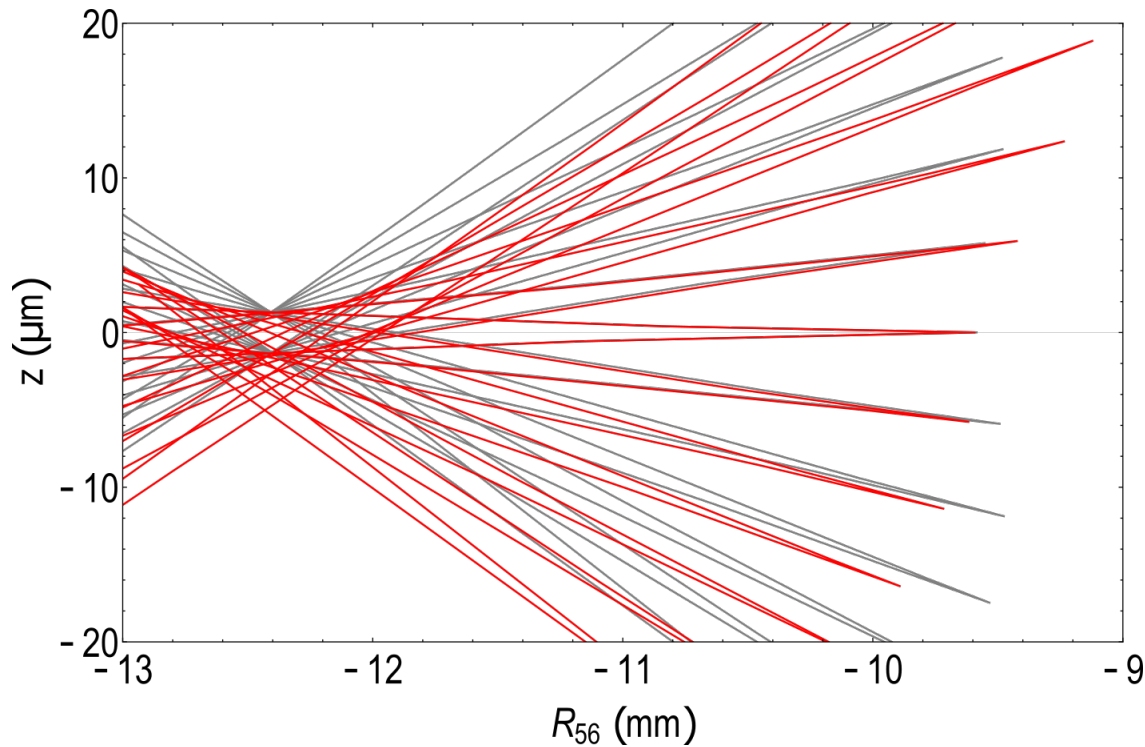
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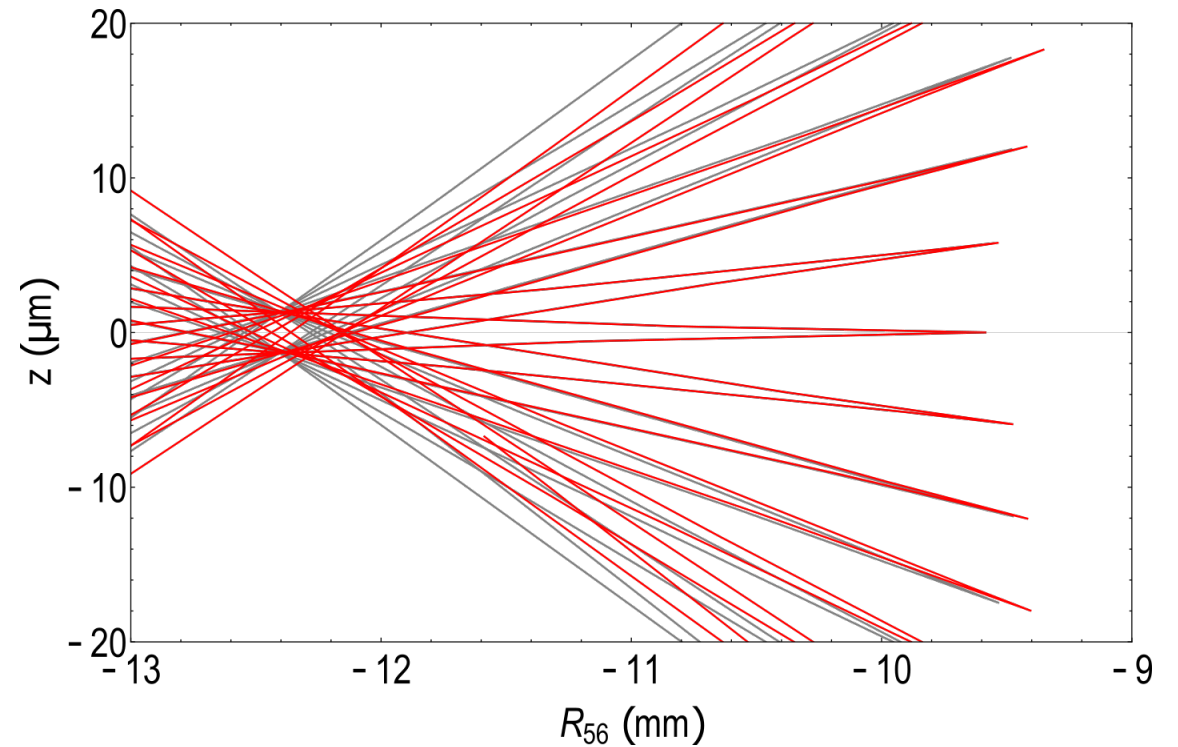
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- Including and varying higher-order effects we can see how the caustic lines change.



$T_{566} = U_{5666} = 0$  mm (gray)  
 $T_{566} = -30$  mm,  $U_{5666} = 0$  mm (red)



$T_{566} = U_{5666} = 0$  mm (gray)  
 $U_{5666} = -2$  m,  $T_{566} = 0$  (red)

- Caustics can form in electron trajectories which are always associated with current spikes.
- Current horns from strong bunch compression can be avoided with higher-order magnetic elements.

I would like to thank:

- Rohan Dowd (Australian Synchrotron)
- David Paganin (Monash University)
- Andrea Latina (CERN)
- Mark Boland (Canadian Light Source)





Australian  
Synchrotron



Ansto



MONASH  
University

# Thank you



Australian  
Synchrotron



Ansto



# Back-up slides

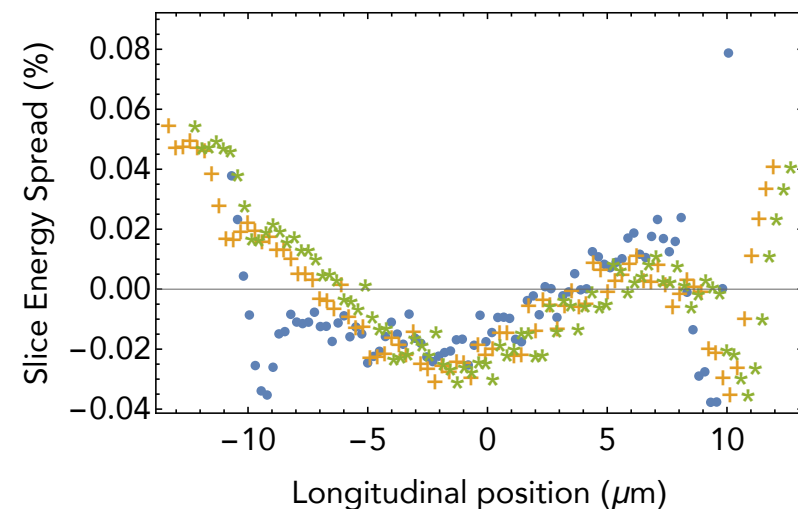
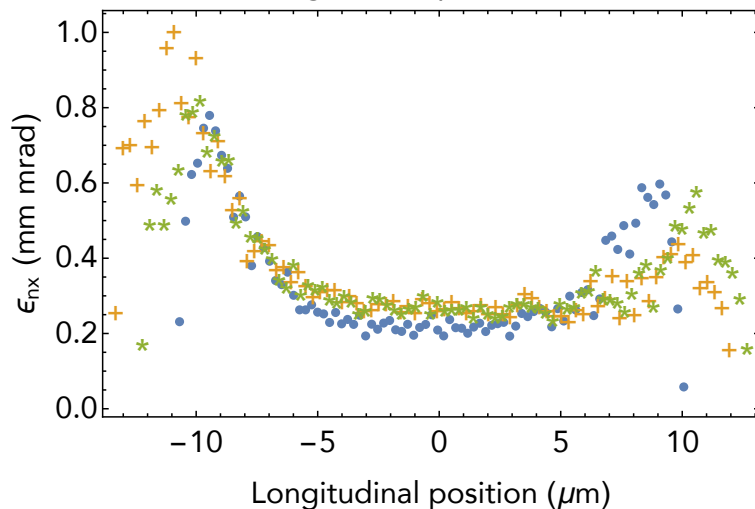
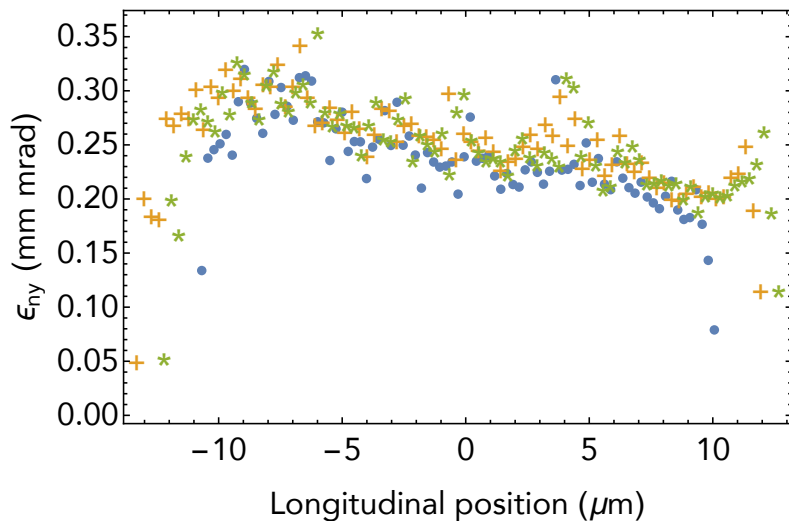
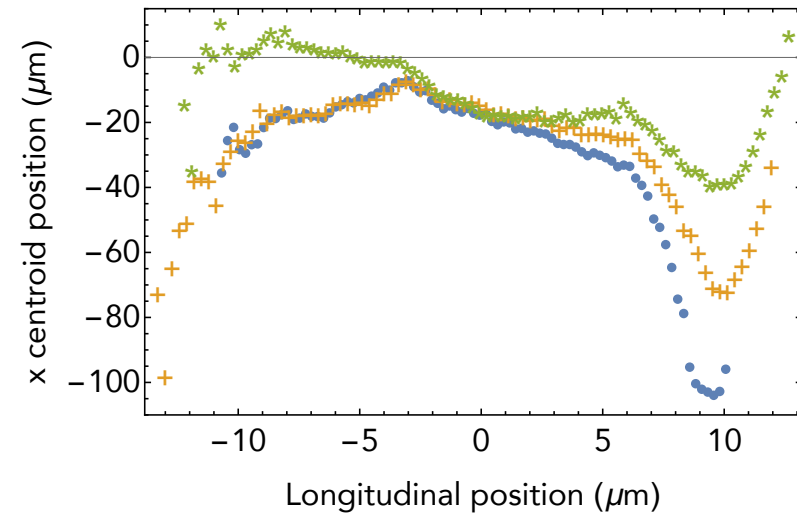
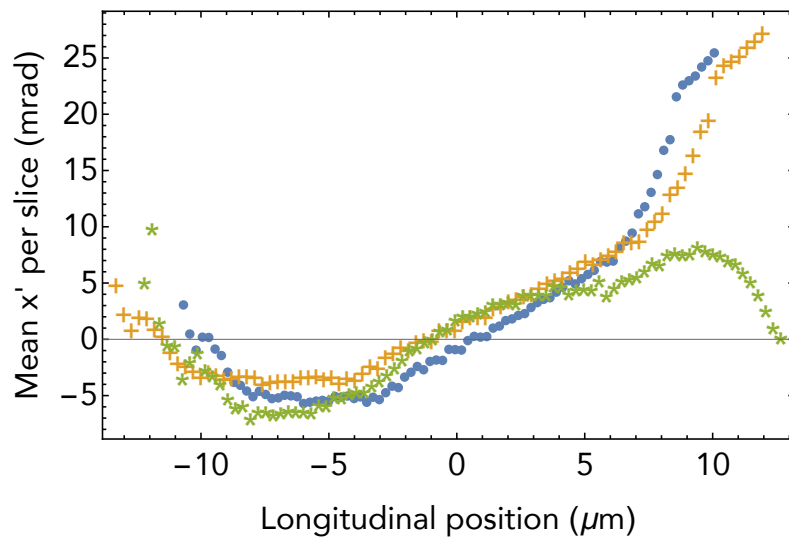


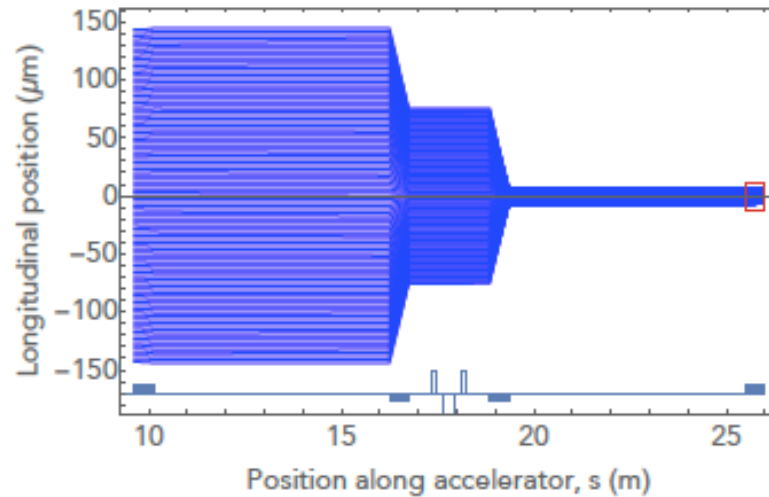
# X-band linac

Without octupole: •

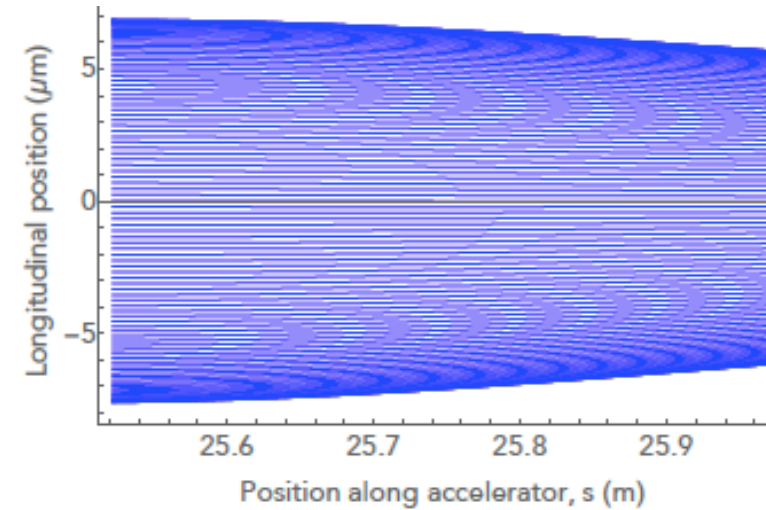
With octupole: +

With octupole and sextupole: \*





(a)



(b)

**Figure 6.8:** Electron trajectories (in  $s$ - $z$  space) through a bunch compressor. (b) shows a close up of the trajectories through the fourth dipole (i.e. region outlined with a red box in (a)). Caustics can be seen forming at head and tail of the bunch in (b).

TABLE I: Beam properties at the end of the final linac section, for (a) Baseline layout, (b) Layout 1: which includes BC1 octupole magnet (Fig. 6a), (c) Layout 2 which includes BC2 sextupole magnet (Fig. 6b).

Parameter	Symbol	Units	Baseline	Layout 1	Layout 2
Bunch length	$\sigma_z$	$\mu\text{m}$	6.65	6.75	6.68
Horizontal bunch size	$\sigma_x$	$\mu\text{m}$	0.376	0.306	0.267
Vertical bunch size	$\sigma_y$	$\mu\text{m}$	0.161	0.162	0.163
Energy spread	$\sigma_{\Delta E/E}$	%	0.0371 (core)	0.0292	0.0281
Peak current	$I_{peak}$	kA	3.02 (core)	3.02	3.09
Total compression ratio	CR	-	121.38 <sup>a</sup>	119.6	120.8
Bunch charge	Q	pC	250	250	250
Electron energy	E	GeV	6.16	6.16	6.16
Projected horizontal emittance	$\epsilon_{n,x}$	mm mrad	1.394	0.974	0.842
Mean horizontal slice emittance	$\epsilon_{s,n,x}$	mm mrad	0.386	0.392	0.377
Projected vertical emittance	$\epsilon_{n,y}$	mm mrad	0.274	0.273	0.274
Mean vertical slice emittance	$\epsilon_{s,n,y}$	mm mrad	0.255	0.249	0.246

<sup>a</sup> Note the bending angles of BC2 were reduced by less than 0.01% to bring the compression ratio down to be in-line with Layout 1 and Layout 2.

